# DG Placement in Radial Distribution Network with Reconfiguration 

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This paper presents a simple method for finding the optimal DG size and optimal DG location in distribution network. By using this method, optimal DG capacity and location are determined considering without network reconfiguration and with network reconfiguration. The method is tested with three test cases: 33-node, 69-node and 117-node IEEE standard network. Result shows that the proposed method is very efficient and competitive with the existing methods available in the literature.

Keywords: Optimal istributedgenerator (DG), Distribution networkreconfiguration, Loss minimization by reconfiguration, Reconfiguration algorithm, 117-bus network.

### 1.0 INTRODUCTION

Loss minimization in distribution power system is one of the biggest challenges before power engineers. It has been estimated that distribution systems cause a loss of about $5 \%-13 \%$ of the total power generated in developing countries. Therefore, the challenges are more pronounced in distribution systems. Basic reason behind these huge power losses is resistive loss, as distribution systems are operated at much lower voltages as compared to transmission systems. The operating current in distribution system is much more than that in transmission systems and hence, larger power loss (active) in distribution systems as compared to transmission systems.

In recent years, the penetration of distributed generator (DG) into distribution systems has also been increasing rapidly in many parts of the world. The main reasons for the increase in penetration are the liberalization of electricity markets, constraints on building new transmission and distribution lines, and environmental concerns. Technological advances in small generators, power electronics, and energy storage devices for transient backup have also accelerated the
penetration of DG into electric power generation plants.

Network reconfiguration is an important optimization tool in distribution network automation systems.With loads prediction system and remote monitoring system, network structure can be reconfigured in real time. By changing open/closed states of some tie and sectionalizing switches, active power losses can be reduced. The other advantages are balancing of overloads, improvement in power supply reliability, etc.

Sivanagaraju et al. [1] presented an application of Genetic Algorithm for radial distribution systems using a chromosome coding method and gene operation strategy. Crossover operations are defined as to exchange between templates while mutation operations are restricted in template. The above strategy greatly reduces infeasible solutions, which are produced during gene operations. Further, a vector-based load flow method for a distribution system is also proposed and the reciprocal value of the active power losses is taken as fitness function. The above measures improve the performance of GA for distribution reconfiguration. Several tests are conducted and

[^0]the results have shown that proposed algorithm has more advantages over previously developed algorithms. Prasad et al. [2] presented genetic algorithm-based network reconfiguration which is proposed for load balancing. Using the proposed technique, the optimal network reconfiguration by load balancing can be obtained with reduced computational effort. The proposed method is applicable in systems with the possibility for on line changing of the topological network structure. Ching-Tzong et al. [3] introduces a hybrid differential evolution (HDE) method for dealing with optimal network reconfiguration aiming power loss reduction. The proposed method determines the proper system topology that reduces the power loss according to a load pattern. This article presents a new approach that employs the HDE algorithm with integer variables to solve the problem. Two other methods, namely the genetic algorithm and the simulated annealing, are also employed to solve the problem. Das [4] presented an algorithm for network reconfiguration based on fuzzy multiobjective approach. Multiple objectives are considered for load balancing among the feeders, i.e. minimum deviation of the nodes voltage, minimize the power loss and branch current constraint violation, while subject to a radial network structure in which all loads must be energized. These objectives are modeled with fuzzy sets to evaluate their imprecise nature and one can provide his or her anticipated value of each objective. These four objectives are first fuzzified and then a fuzzy satisfaction objective function is formed and maximized for each tie-switch operation. Heuristic rules are also incorporated in the algorithm for minimizing the number of tie-switch operation. Subrahmanyam et al. [5] presents a simple reconfiguration algorithm that is specially suited for balanced and unbalanced radial distribution systems. The proposed algorithm involves less complex mathematical expressions, and a more efficient network configuration can be obtained with reduced power losses. The choice of the switches to be closed is based on the calculation of bus voltages and the minimum total system losses using a power flow program. Lin et al. [6] have applied refined genetic algorithm to network
reconfiguration problem for reduction of resistive line losses. In this method, the authors have refined the conventional crossover and mutation scheme by a competition mechanism to avoid premature convergence. Mendoza et al. [7] have proposed and evaluated a method that improves the adaptability and efficiency of genetic algorithms (GAs) when applied to the minimal loss reconfiguration problem. This research reduces the searching space (population) when a new codification strategy and novel genetic operators, called accentuated crossover and directed mutation, are used. This allows a drastic reduction of the computational time and minimizes the memory requirements, ensuring a efficiency search when compared to current GA reconfiguration techniques. Kumar Injeti et al. [8] had presented planning and operation of active distribution networks, with respect to placement and sizing of Distributed Generators with the help of a new methodology. DG unit placement and sizing were calculated using fuzzy logic and new analytical method, respectively. Vinoth Kumar et al. [9] had investigated the problem of multiple distributed generators (DG units) placement to achieve a high loss reduction in large-scale primary distribution networks. An improved analytical (IA) method is proposed in that work. This method is based on improved analytical expressions to calculate the optimal size of four different DG types, and methodology is proposed to identify the best location for DG allocation. Naresh et al. [10] had presented and analytical method for DG placement in radial distribution network. Analytical expressions have presented to calculate the optimal size and an effective methodology to identify the corresponding optimum location for DG placement for minimizing the total power losses in primary distribution systems. The analytical expression and the methodology are based on the exact loss formula. The effect of size and location of DG with respect to loss in the network is also examined in detail. Khorshidi et al. [11] has presented an approach for distribution reconfiguration considering Distributed Generators (DGs). The objective function is summation of electrical power losses of the whole system. A Tabu search optimization
is used to solve the optimal operation problem. Rugthaicharoencheep et al. [12] had presented a feeder reconfiguration problem to the distribution system with dispatchable distributed generators. A Tabu search algorithm is applied to search for the on-off patterns of the sectionalizing switches and tie switches to obtain the minimum total power loss, whereas the dispatch schedule of the distributed generators which gives the minimum total cost of generation is solved by optimal power flow.

In this paper, a new method for feeder reconfiguration has been used. This paper presents a minimal tree search to find the possible switching options for loss reduction. A simple loss change formula is developed to determine the switching option that gives a maximum reduction in losses. The proposed method is found to be efficient and obtains the optimal or near optimal configuration for loss minimization. In this paper, a simple algorithm to calculate optimum size and location for DG placement is proposed. The DG is considered to be located in the primary distribution system and the objective of DG placement is to reduce the losses. The cost of DG and the other associated benefits have not been considered while solving the location and sizing problem. The sizing and placement of DG are based on single instantaneous demand at peak, when the losses are maximum. The proposed methodology is suitable for allocation of single DG in a given distribution network.

### 2.0 DISTRIBUTION NETWORK RECONFIGURATION

Feeder reconfiguration for loss minimization in distribution systems is realized by changing the status of sectionalizing and tie switches. Most electric distribution networks are operated radially. Configuration alterations are performed by changing the state of network switches in such a way that radiality is always preserved. The optimal operating condition of distribution networks is obtained when line losses are minimized without any violations of branchloading and voltage limits. Therefore, feeder reconfiguration is implemented to minimize
real power losses and at the same time alleviate transformer overload, feeder thermal overload and abnormal voltages of the system. There are two types of switches in the system:

1. normally closed switches connecting the line sections called sectionalizing switches
2. normally open switches on the tie-lines connecting either two primary feeders or two substations, or loop-type laterals called tie-switches. The change in network configuration is achieved by opening or closing of these two types of switches in such a way that the 'radiality' of the network is maintained.

### 2.1 Formulation of Loss Reduction Problem

Feeder reconfiguration is performed by changing the open/closed status of the sectionalizing and ties switches. The system is reconfigured for many purposes. In system reconfiguration, a whole feeder or part of a feeder is transferred to another feeder by closing a tie switch connecting the two, while an appropriate sectionalizing switch must be opened to preserve the radial structure. The loss minimization problem to be addressed in this work is to determine the open/closed states of the tie and sectionalizing switches in order to achieve a maximum reduction in power losses. The change in losses can be easily estimated from the two power flow solutions, which are obtained before and after feeder reconfiguration. However, the number of switching options even for a moderate size distribution system is so large and therefore a large number of load flow solutions have to be executed for all the possible options. It becomes not only inefficient from a computational point of view, but also unrealistic as a feeder reconfiguration strategy. Therefore, it is desirable to propose a method that can provide a criterion that may be used to eliminate the undesirable switching options.

### 2.2 Objective Function for Loss Minimization by Reconfiguration

To solve the loss reduction problem, it is necessary to calculate the change of losses by
various switching options and to select the switching candidates which give the maximum loss reduction. Active and reactive power losses in the network can be calculated using the following equations.
$\mathrm{LP}_{\mathrm{ij}}=\frac{\mathrm{R}_{\mathrm{ij}}\left[\mathrm{P}_{\mathrm{ij}}{ }^{2}+\mathrm{Q}_{\mathrm{j} j}{ }^{2}\right]}{\left|\mathrm{V}_{\mathrm{ij}}{ }^{2}\right|}$
$\mathrm{LQ}_{\mathrm{jj}}=\frac{\mathrm{X}_{\mathrm{ij}}\left[\mathrm{P}_{\mathrm{ij}}{ }^{2}+\mathrm{Q}_{\mathrm{ij}}{ }^{2}\right]}{\left|\mathrm{V}_{\mathrm{ij}}{ }^{2}\right|}$
where $L P_{i \mathrm{ij}}$ and $\mathrm{LQ}_{\mathrm{ij}}$ are active and reactive power losses in the branch jj . $\mathrm{R}_{\mathrm{ij}}$ and $\mathrm{X}_{\mathrm{ij}}$ are resistance and reactance of branch $\mathrm{jj} . \mathrm{V}_{\mathrm{ij}}$ is the voltage of sending node. It is clear from (1) that the power loss in the system is inversely proportional to the voltage square of sending node. Sending node voltage can be calculated using following equation:
$\mathrm{V}_{\mathrm{m} 2}=\mathrm{V}_{\mathrm{m} 1}-\mathrm{I}_{(\mathrm{j})} \times \mathrm{Z}_{(\mathrm{j})}$
where $\mathrm{V}_{\mathrm{m} 2}$ is the voltage of load side node of branch jj , $\mathrm{V}_{\mathrm{m} 1}$ is source side node voltage of branch jj. By selecting proper combination of switches, source side voltage can be improved which in turn automatically improves voltage of receiving node, as well as the voltage profile of follower branches.

The tie switch or sectionalizing switch can be sorted in descending order as per the voltage difference. The switch with the highest voltage difference should be operated first. To reduce total power loss, lower voltage side branch has to be opened first. This will continue till the voltage difference between open switches is less than 0.001 pu. The steps used to determine the branch to be exchanged give the maximum loss reduction, which is described in next section.

### 2.3 Reconfiguration Algorithm

1. Run the load flow program to find out total power loss and voltage across open switches.
2. Check weather voltage difference across open switch is less than 0.001 or not if yes
then select these switchs and save its value in array variable nmb .
3. Short array nmb in descending order to find switch with maximum voltage difference.
4. Start with the first switch of nmb relay. Close that switch and open branch at lower voltage side.
5. Run load flow and calculate power loss.
6. Continue step no 4 until power loss of new switch combination is greater than previous combination. With the constraint that source node should not be opened, network should be radial and all load must be served.
7. Again repeat steps no 5 and 6 for other variables of nmb array.
8. After changing combination of all open switches (one cycle of reconfiguration) ,compare power loss of new network with previous network power loss if it is less then again start from step 1.
9. If after reconfiguration loss of network is same as previous network, then stop repeating reconfiguration and print results.

Flow chart for the same is shown in Figure 1.

### 2.4 Results for Reconfiguration

Results for power loss after reconfiguration for 32, 68 and 117 bus have shown in Table 1.

| TABLE 1 |  |  |  |
| :---: | :---: | :---: | :---: |
| RESULTS FOR RECONFIGURATION |  |  |  |
| Radial <br> network | Power loss <br> actual <br> (kW) | Loss $\mathbf{( k W )}$ <br> after rec <br> existing <br> method [1] | Loss $\mathbf{( k W )}$ <br> after rec <br> proposed <br> method |
| 32 Bus | 211 | 139.5 | 139.5 |
| 68 Bus | 224 | 98 | 98 |
| 117 Bus | 1250 | 859 | 859 |

### 3.0 DISTRIBUTED GENERATOR PLACEMENT

Distributed generation is an electric power source connected directly to the distribution

network or customer side of the meter [10]. It may be understood in simple term as smallscale electricity generation. The definition of distributed generation takes different forms in different markets and countries, and is defined differently by different agencies. International Energy Agency (IEA) defines Distributed generation as generating plant serving a customer on-site or providing support to a distribution network, connected to the grid at distribution-level voltages. CIGRE defines DG as the generation, which has the following
characteristics: it is not centrally planned; it is not centrally dispatched at present; it is usually connected to the distribution network; it is smaller than $50-100 \mathrm{MW}$. Other organization like Electric Power Research Institute defines distributed generation as generation from a few kilowatts up to 50 MW [10]. In general, DG means small-scale generation.

There are a number of DG technologies available in the market today and few are still in research and development stage. Some currently available
technologies are reciprocating engines, micro turbines, combustion gas turbines, fuel cells, photovoltaic, and wind turbines. Each one of these technologies has its own benefits and characteristics. Among all the DG, diesel or gas reciprocating engines and gas turbines make up most of the capacity installed so far. Simultaneously, new DG technology like micro turbine is introduced and an older technology like reciprocating engine is improved [10]. Fuel cells are technology for the future. However, there are some prototype demonstration projects. The costs of photovoltaic systems are expected to fall continuously over the next decade.

DG also has several benefits like reducing energy costs through combined heat and power generation, avoiding electricity transmission costs and less exposure to price volatility. Although the DG is considered as a viable solution, it creates auxiliary problems towards the utility. Moreover, there are many problems, e.g. DG integration into grid, pricing, change in protection scheme, nuisance tripping, etc. that needs to be addressed. Furthermore, the type of DG technology adopted will have a significant impact on the solution approach. In this study, it is assumed that DGs are capable of supplying real power only.

### 3.1 Objective Function for Loss Minimization by DG

To find out the optimum loss reduction, it is necessary to calculate the changes of losses after inserting DG into the system. By comparing losses of different capacity of DG at different locations, the optimum capacity of DG can be found out which can reduce the losses to minimum. If DGs of capacity $P_{D G}$ are installed at branch $i$, then total power of that branch will be given as:
$P_{i}=P_{i}^{\text {Act }}-P_{D G}$

Value of $\mathrm{P}_{\mathrm{i}}$ will start increasing in negative direction when value of $\mathrm{P}_{\mathrm{DG}}$ will become more than actual value of connected load $\mathrm{P}_{\mathrm{i}}^{\text {Act }}$. By replacing the actual load of branch with this new
load $P_{i}$, new load data can be obtained. From new load data power loss of network can be found out by forward backward swap method. This process will be repeated for different capacity of load varying from 10 kW to maximum or until minimum loss condition occurs on that node. This will give the optimum DG capacity for that node.

The above-mentioned processes for all nodes have to be repeated one by one to find out optimum DG capacity and minimum loss for each node. By comparing these values minimum loss condition for network can be found out and optimum DG capacity for that minimum loss can be obtained.

### 3.2 The Algorithm for DG Placement

1. Run the load flow program to find out total power loss and voltage across open switches.
2. Start connecting DG from the first receiving node 2 and is continued till the last receiving node.
3. Consider loss before DG placement as minimum loss (loss min) for that node.
4. Install DG of starting capacity (variable DGC) from 10 kW . Loop variable $\mathrm{kkk}=1$.
5. Subtract installed DG value (DGC) from the connected load.
6. Run load flow and calculate power loss.
7. If power loss is less than minimum loss, then consider power loss with this DG as minimum loss. Store capacity of DG in variable sub.
8. If kkk (DG capacity loop count) $>2$ and loss of (kkk) > loss of (kkk-1) and loss of (kkk-1) > loss of (kkk-2) then stop increasing DG capacity for that node and go to step 10 .
9. If max DG capacity not reached, then increase DGC by 10 and kkk by 1 go to step no. 5 .
10. Print Loss and DG capacity.
11. If final node is not reached, then increase nmin by 1 and go to step no. 3 .

Flow chart for the same is presented in Figure 2. Results after one DG placement is shown in Table 2.


| TABLE 2 |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| RESULTS FOR DG PLACEMENT |  |  |  |  |
|  | Without DG | Only one DG |  |  |
| System | Total loss | Node | $\begin{gathered} \text { DG } \\ \text { capacity } \end{gathered}$ | Total loss |
|  |  | Proposed Method |  |  |
| 32 Bus | 211 | 6 | 2590 | 110.99 |
| 68 Bus | 224 | 61 | 1870 | 83.312 |
| 117 Bus | 1250 | 74 | 2980 | 996.81 |
|  |  | Other Method [8] |  |  |
| 32 Bus | 211 | 6 | 2590 | 110.99 |
| 68 Bus | 224 | 61 | 1870 | 83.312 |
| 117 Bus | 1250 | 74 | 2980 | 996.81 |

### 4.0 DISTRIBUTED GENERATOR PLACEMENT AFTER RECONFIGURATION

After reconfiguration, algorithm and flow chart for DG placement will remain same. Then repeat the step described in Section 2. Afterwards, the data of the reconfigured system will become the base data for the DG placement calculations. By following above-mention steps, optimum capacity of DG and its location can be obtained.

### 5.0 CASE STUDIES

To demonstrate the effectiveness of the proposed method, three test cases have been selected. The first test case is a 32 -bus distribution feeder. The second and third test cases are for 68 and 117 bus distribution system, respectively. Tables 3, 4 and 5 gives results for 32 bus, 68 bus and 117 bus cases, respectively. In all these cases value of DG before and after reconfiguration has been compared. It has been observed that on any node after reaching to optimum capacity of DG if the value of injected DG power is increased, further loss of network starts increasing. Same results have shown for 32 bus system in Figure 3. Comparison between DG capacity for system without reconfiguration and system with reconfiguration is shown in Table 6.

| TABLE 3 |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| RESULTS FOR 32-BUS NETWORK |  |  |  |  |
|  | Before reconfiguration DG capacity |  | After reconfiguration DG capacity |  |
| Node No. | $\begin{gathered} \text { DG } \\ \text { capacity } \end{gathered}$ $(\mathbf{k W})$ | $\begin{aligned} & \text { Loss } \\ & \text { (kW) } \end{aligned}$ | DG capacity (kW) | $\begin{aligned} & \text { Loss } \\ & \text { (kW) } \end{aligned}$ |
| 2 | 4100 | 200.991 | 3980 | 130.336 |
| 3 | 3650 | 160.489 | 2690 | 112.386 |
| 4 | 3180 | 147.857 | 2190 | 110.187 |
| 5 | 2910 | 135.804 | 1910 | 107.752 |
| 6 | 2590 | 110.992 | 1620 | 101.99 |
| 7 | 2460 | 111.968 | 1500 | 104.396 |
| 8 | 1790 | 118.093 | 960 | 112.787 |
| 9 | 1560 | 121.357 | 860 | 113.544 |
| 10 | 1400 | 123.678 | 730 | 120.38 |
| 11 | 1370 | 124.148 | 750 | 119.801 |
| 12 | 1330 | 125.203 | 800 | 118.749 |
| 13 | 1170 | 129.401 | 660 | 121.255 |
| 14 | 1110 | 130.996 | 610 | 122.156 |
| 15 | 1060 | 133.465 | 710 | 114.708 |
| 16 | 1000 | 136.723 | 670 | 115.206 |
| 17 | 900 | 142.534 | 600 | 116.39 |
| 18 | 850 | 145.682 | 570 | 117.207 |
| 19 | 1720 | 206.148 | 2310 | 130.92 |
| 20 | 480 | 208.345 | 1390 | 117.257 |
| 21 | 420 | 208.452 | 1340 | 113.918 |
| 22 | 340 | 208.792 | 1120 | 115.814 |
| 23 | 2470 | 169.786 | 1930 | 114.733 |
| 24 | 1710 | 173.767 | 1420 | 114.161 |
| 25 | 1300 | 179.324 | 1100 | 117.048 |
| 26 | 2450 | 112.898 | 1560 | 101.51 |
| 27 | 2280 | 115.313 | 1480 | 101.03 |
| 28 | 1850 | 120.96 | 1260 | 99.291 |
| 29 | 1640 | 123.227 | 1150 | 98.076 |
| 30 | 1540 | 125.115 | 1090 | 98.04 |
| 31 | 1350 | 131.175 | 970 | 100.166 |
| 32 | 1300 | 133.543 | 930 | 101.27 |
| 33 | 1230 | 137.281 | 550 | 118.027 |



FIG. 3 GRAPH POWER LOSS VS DG CAPACITY

| TABLE 4 |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| RESULTS FOR 68-BUS NETWORK |  |  |  |  |
|  | Before reconfiguration DG capacity |  | After reconfiguration DG capacity |  |
| Node No. | DG capacity (kW) | $\begin{aligned} & \text { Loss } \\ & \text { (kW) } \end{aligned}$ | DG capacity (kW) (kW) | $\begin{aligned} & \text { Loss } \\ & \text { (kW) } \end{aligned}$ |
| 2 | 4100 | 225.023 | 4080 | 98.638 |
| 3 | 4100 | 224.904 | 4080 | 98.534 |
| 4 | 4100 | 224.703 | 3550 | 98.426 |
| 5 | 3300 | 223.167 | 1080 | 98.53 |
| 6 | 3110 | 200.816 | 710 | 97.489 |
| 7 | 3040 | 178.454 | 690 | 96.395 |
| 8 | 3020 | 173.321 | 680 | 96.164 |
| 9 | 3000 | 170.828 | 560 | 96.091 |
| 10 | 1960 | 181.197 | 540 | 95.312 |
| 11 | 1850 | 182.102 | 540 | 95.152 |
| 12 | 1500 | 186.037 | 450 | 95.286 |
| 13 | 1180 | 191.301 | 330 | 96.183 |
| 14 | 1000 | 194.05 | 260 | 96.72 |
| 15 | 880 | 195.631 | 740 | 90.305 |
| 16 | 860 | 195.83 | 730 | 89.738 |
| 17 | 830 | 196.344 | 720 | 88.821 |
| 18 | 830 | 196.355 | 720 | 88.812 |
| 19 | 800 | 197.143 | 690 | 88.36 |
| 20 | 780 | 197.604 | 680 | 88.063 |
| 21 | 750 | 198.293 | 660 | 87.578 |
| 22 | 750 | 198.337 | 660 | 87.571 |


| 23 | 730 | 198.804 | 650 | 87.5 |
| :---: | :---: | :---: | :---: | :---: |
| 24 | 700 | 199.773 | 630 | 87.33 |
| 25 | 640 | 201.779 | 590 | 87.055 |
| 26 | 620 | 202.511 | 570 | 86.919 |
| 27 | 610 | 202.921 | 570 | 86.855 |
| 28 | 1520 | 225.055 | 1420 | 98.666 |
| 29 | 190 | 225.126 | 180 | 98.727 |
| 30 | 60 | 225.131 | 60 | 98.731 |
| 31 | 60 | 225.131 | 60 | 98.73 |
| 32 | 50 | 225.128 | 50 | 98.727 |
| 33 | 50 | 225.125 | 50 | 98.72 |
| 34 | 40 | 225.127 | 40 | 98.715 |
| 35 | 30 | 225.136 | 30 | 98.72 |
| 36 | 1630 | 225.042 | 2000 | 98.592 |
| 37 | 290 | 225.106 | 960 | 98.358 |
| 38 | 200 | 225.101 | 880 | 97.906 |
| 39 | 190 | 225.098 | 880 | 97.776 |
| 40 | 190 | 225.098 | 870 | 97.768 |
| 41 | 110 | 225.077 | 800 | 94.986 |
| 42 | 100 | 225.064 | 790 | 93.81 |
| 43 | 100 | 225.062 | 790 | 93.655 |
| 44 | 100 | 225.062 | 790 | 93.621 |
| 45 | 100 | 225.059 | 780 | 93.216 |
| 46 | 100 | 225.059 | 780 | 93.212 |
| 47 | 2760 | 224.809 | 3030 | 98.339 |
| 48 | 80 | 224.569 | 80 | 93.512 |
| 49 | 820 | 223.506 | 2260 | 86.154 |
| 50 | 750 | 223.512 | 2180 | 84.432 |
| 51 | 2740 | 178.066 | 620 | 96.38 |
| 52 | 2050 | 189.857 | 470 | 96.977 |
| 53 | 2830 | 167.33 | 580 | 96.443 |
| 54 | 2690 | 163.039 | 500 | 96.738 |
| 55 | 2540 | 157.059 | 410 | 97.062 |
| 56 | 2420 | 151.232 | 350 | 97.315 |
| 57 | 2090 | 118.721 | 190 | 97.971 |
| 58 | 2000 | 103.444 | 150 | 98.114 |
| 59 | 1960 | 97.667 | 1520 | 59.993 |
| 60 | 1920 | 91.464 | 1480 | 56.096 |
| 61 | 1870 | 83.312 | 1440 | 50.989 |


| 62 | 1850 | 84.816 | 450 | 87.536 |
| :---: | :---: | :---: | :---: | :---: |
| 63 | 1810 | 87.07 | 450 | 87.374 |
| 64 | 1650 | 96.702 | 490 | 86.488 |
| 65 | 1440 | 112.234 | $\mathbf{6 0}$ | $\mathbf{8 3 . 4 3 2}$ |
| 66 | 1680 | 185.912 | 490 | 95.445 |
| 67 | 1680 | 186.002 | 490 | 95.451 |
| 68 | 1190 | 193.789 | 370 | 95.849 |
| 69 | 1190 | 193.834 | 370 | 95.853 |


| TABLE 5 |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| RESULTS FOR 117-BUS NETWORK |  |  |  |  |
|  | Before reconfiguration DG capacity |  | After reconfiguration DG capacity |  |
| Node No. | DG capacity (kW) | $\begin{aligned} & \text { Loss } \\ & (\mathbf{k W}) \end{aligned}$ | DG capacity (kW) | $\begin{aligned} & \text { Loss } \\ & (\mathbf{k W}) \end{aligned}$ |
| 2 | 5100 | 1252.176 | 4100 | 837.662 |
| 3 | 5100 | 1259.279 | 4100 | 842.252 |
| 4 | 5100 | 1228.572 | 4100 | 817.685 |
| 5 | 5100 | 1231.381 | 4100 | 816.164 |
| 6 | 5100 | 1234.282 | 4100 | 814.721 |
| 7 | 5100 | 1237.284 | 4100 | 813.473 |
| 8 | 5100 | 1241.034 | 4100 | 812.113 |
| 9 | 5100 | 1245.459 | 4100 | 813.13 |
| 10 | 5100 | 1254.904 | 3570 | 837.475 |
| 11 | 3060 | 1253.395 | 2940 | 836.241 |
| 12 | 3060 | 1260.745 | 2050 | 841.302 |
| 13 | 3060 | 1263.493 | 1710 | 843.077 |
| 14 | 3060 | 1265.773 | 1440 | 844.503 |
| 15 | 3060 | 1267.416 | 1270 | 845.647 |
| 16 | 3060 | 1268.763 | 1140 | 846.571 |
| 17 | 3060 | 1269.833 | 1030 | 847.314 |
| 18 | 2390 | 1252.334 | 2170 | 837.723 |
| 19 | 2200 | 1251.07 | 1970 | 837.578 |
| 20 | 2010 | 1249.897 | 1750 | 837.683 |
| 21 | 2010 | 1250.927 | 1570 | 839.3 |
| 22 | 2010 | 1252.222 | 1420 | 841.023 |
| 23 | 2010 | 1258.258 | 660 | 850.012 |


| 24 | 2010 | 1258.864 | 2960 | 816.289 |
| :---: | :---: | :---: | :---: | :---: |
| 25 | 2010 | 1259.411 | 2670 | 815.66 |
| 26 | 2010 | 1260.385 | 740 | 849.819 |
| 27 | 2010 | 1261.296 | 810 | 848.955 |
| 29 | 5100 | 1221.215 | 4100 | 814.629 |
| 30 | 5100 | 1215.923 | 4100 | 812.68 |
| 31 | 5100 | 1191.997 | 4100 | 802.606 |
| 32 | 5100 | 1170.72 | 3530 | 811.735 |
| 33 | 4750 | 1164.331 | 2950 | 816.861 |
| 34 | 4190 | 1159.229 | 2320 | 824.56 |
| 35 | 3800 | 1154.001 | 1910 | 830.083 |
| 36 | 3550 | 1150.645 | 2100 | 811.986 |
| 37 | 3550 | 1216.327 | 3815 | 806.517 |
| 38 | 3550 | 1227.914 | 3190 | 810.219 |
| 40 | 3550 | 1231.111 | 2170 | 841.769 |
| 41 | 2710 | 1230.575 | 1290 | 848.572 |
| 42 | 2350 | 1227.484 | 2400 | 824.632 |
| 43 | 2350 | 1227.613 | 1960 | 826.772 |
| 44 | 2350 | 1231.238 | 1180 | 832.993 |
| 45 | 2350 | 1235.864 | 520 | 851.499 |
| 46 | 2350 | 1238.592 | 570 | 851.012 |
| 47 | 2350 | 1241.761 | 620 | 850.445 |
| 48 | 2350 | 1244.115 | 670 | 849.991 |
| 49 | 3270 | 1146.77 | 1960 | 810.608 |
| 50 | 3150 | 1144.607 | 1890 | 809.954 |
| 51 | 3010 | 1142.2 | 1810 | 809.377 |
| 52 | 2880 | 1140.42 | 1740 | 809.212 |
| 53 | 2880 | 1148.08 | 1320 | 828.171 |
| 54 | 2880 | 1152.342 | 1390 | 826.839 |
| 55 | 2880 | 1171.365 | 1160 | 832.099 |
| 56 | 2170 | 1165.032 | 1680 | 822.092 |
| 58 | 2170 | 1247.69 | 2420 | 834.372 |
| 59 | 2170 | 1252.137 | 1660 | 837.839 |
| 60 | 2170 | 1253.46 | 1340 | 838.909 |
| 61 | 2170 | 1254.143 | 1060 | 839.55 |
| 62 | 2170 | 1255.984 | 940 | 841.254 |
| 63 | 2170 | 1257.442 | 840 | 842.615 |
| 64 | 2170 | 1258.409 | 790 | 843.508 |
| 65 | 2170 | 1259.854 | 1980 | 820.367 |


| 66 | 2170 | 1263.939 | 4100 | 847.941 |
| :---: | :---: | :---: | :---: | :---: |
| 67 | 5100 | 1208.917 | 4100 | 804.842 |
| 68 | 5100 | 1146.097 | 4100 | 774.11 |
| 69 | 5100 | 1129.025 | 3870 | 779.251 |
| 70 | 4310 | 1108.861 | 2860 | 787.405 |
| 71 | 3750 | 1077.946 | 2300 | 788.415 |
| 72 | 3470 | 1054.179 | 2050 | 787.201 |
| 73 | 3050 | 1001.141 | 1700 | 782.508 |
| 74 | 2980 | 996.81 | 1640 | 783.665 |
| 75 | 2980 | 998.066 | 1660 | 794.672 |
| 76 | 2980 | 1000.398 | 1860 | 787.774 |
| 77 | 2980 | 1002.056 | 2240 | 762.334 |
| 78 | 2980 | 1012.812 | 2420 | 759.511 |
| 79 | 2980 | 1036.258 | 1890 | 779.122 |
| 80 | 2980 | 1041.562 | 1370 | 801.497 |
| 81 | 2980 | 1206.856 | 4000 | 758.194 |
| 82 | 3070 | 1203.287 | 3740 | 746.165 |
| 83 | 3070 | 1205.763 | 3260 | 754.965 |
| 84 | 3070 | 1212.328 | 2730 | 768.669 |
| 85 | 3070 | 1216.468 | 2470 | 776.272 |
| 86 | 3070 | 1222.986 | 1490 | 805.281 |
| 87 | 3070 | 1229.349 | 1380 | 809.295 |
| 88 | 3070 | 1233.172 | 1300 | 811.912 |
| 89 | 2670 | 1211.237 | 3400 | 748.174 |
| 90 | 2670 | 1221.348 | 3040 | 752.976 |
| 91 | 2670 | 1227.917 | 2800 | 755.885 |
| 93 | 3310 | 1173.508 | 3310 | 772.723 |
| 94 | 3310 | 1174.436 | 2750 | 768.524 |
| 95 | 2680 | 1173.84 | 2560 | 763.878 |
| 96 | 2680 | 1185.402 | 2240 | 774.28 |
| 97 | 2680 | 1195.222 | 1990 | 783.181 |
| 98 | 2680 | 1202.679 | 1800 | 789.974 |
| 99 | 2680 | 1214.913 | 1500 | 801.144 |
| 100 | 2510 | 1175.485 | 2400 | 764.383 |
| 101 | 2510 | 1180.751 | 2230 | 768.527 |
| 102 | 2510 | 1188.372 | 2050 | 775.122 |
| 103 | 2510 | 1209.613 | 1570 | 793.561 |
| 105 | 2510 | 1261.038 | 4100 | 843.256 |
| 106 | 5100 | 1228.64 | 4010 | 830.055 |


| 107 | 4890 | 1205.642 | 3540 | 821.869 |
| :--- | :--- | :--- | :--- | :--- |
| 108 | 4440 | 1176.7 | 3020 | 813.493 |
| 109 | 3900 | 1135.165 | 2490 | 803.51 |
| 110 | 3770 | 1121.881 | 2370 | 800.376 |
| 111 | 3550 | 1097.771 | 2180 | 794.957 |
| 112 | 3460 | 1087.484 | 2110 | 792.794 |
| 113 | 3210 | 1073.55 | 1890 | 793.425 |
| 114 | 3110 | 1069.51 | 1790 | 795.527 |
| 115 | 3110 | 1069.554 | 1790 | 773.885 |
| 116 | 3110 | 1075.235 | 1710 | 773.528 |
| 117 | 3110 | 1080.191 | 1690 | 777.154 |
| 118 | 3110 | 1093.456 | 1580 | 782.239 |
| 119 | 3110 | 1272.39 | 2520 | 822.427 |
| 120 | 3110 | 1272.839 | 2380 | 816.737 |
| 121 | 3110 | 1273.477 | 2200 | 806.279 |
| 122 | 3110 | 1274.352 | 2050 | 797.247 |
| 123 | 3110 | 1275.116 | 1920 | 787.125 |


| TABLE 6 |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| DG CAPACITY AFTER AND BEFORE <br> RECONFIGURATION |  |  |  |  |
|  | DG before reconf |  | DG after reconf |  |
| System | DG <br> capacity | Total <br> loss | DG <br> capacity | Total <br> loss |
| 32 Bus | 2590 | 110.99 | 1090 | 98.037 |
| 68 Bus | 1870 | 83.312 | 1440 | 50.989 |
| 117 Bus | 2980 | 996.81 | 1640 | 783.67 |

### 6.0 CONCLUSIONS

In this paper, a novel algorithm is proposed to calculate the optimum size of DG at various nodes and methodology to identify the optimum location corresponding to the optimum size for reduction of total power losses in distribution system. The proposed methodology has been tested in 32 bus, 68 bus and 117 bus test systems and satisfactory results have been obtained. It identifies the best location for single DG placement in order to minimize the total power losses. The same methodology has been used to calculate optimum size and location of DG after
reconfiguring system. From the results, it is clear that DG capacity after reconfiguration reduces drastically compared to the DG capacity before reconfiguration.

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