# Implementations of Sweep Algorithm For Load Flow Analysis in Radial Distribution Networks 

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#### Abstract

Power system is the most complex man made inter connected system with the combination of power generation, transmission and distribution to the consumer loads. In order to determine the behavior of the entire system i.e., planning and design, economic operation, stability. etc of the power system the power flow or load studies plays vital role. By using this power flow solution we obtain magnitude and phase angle of voltage at each bus, real and reactive power flowing through the branches by using conventional iterative techniques like Gauss-seidal, Newton Raphson method, Fast decoupled methods. This paper gives the complete load flow analysis of a radial distribution network with a proposed simple backward/forward sweep algorithm method which gives better convergence and takes full advantage of the radial structure of distribution systems tested for the IEEE 33 bus and IEEE 69 bus system implemented in MATLAB ${ }^{T M}$ code.


Keywords: Distribution systems, radial distribution systems, power flow analysis, algorithm.

### 1.0 INTRODUCTION:

Electrical energy is the essential ingredient for the development of industrial, domestic and all for the existence of the civilized world today. As the power demand is increasing day by day it is necessity to generate the power sufficiently from all the sources and transmit to the distributed system with the help of inter connected tie lines. Distribution system is the part of the power system gives the necessary information helps for the reliable power supply to consumers. Distribution of electric power is done by distribution networks and distribution networks consist of following main parts distribution substation, Primary distribution feeder, Distribution Transformer, Distributors, and Service mains. There are three basic types of distribution system designs: 1. Radial distribution system: The radial distribution is the cheapest to build, and is widely used in sparsely populated areas (Figure 1). A radial
system has only one power source for a group of customers. 2. Loop distribution system: A loop system, as the name implies, loops through the service area and returns to the original point (Figure 2). The loop is usually tied into an alternate power source. By placing switches in strategic locations, the utility can supply power to the customer from either direction. If one source of power fails, switches are thrown (automatically or manually), and power can be fed to customers from the other source. The loop system is more expensive than the radial because more switches and conductors are required, but the resultant improved system reliability is often worth the price. 3. Network distribution system: Network systems are the most complicated and are interlocking loop systems (Figure 3). A given customer can be supplied from two, three, four, or more different power supplies. Obviously, the big advantage of such a system is added reliability. However, it is also the most expensive.

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A feeder brings power from substation to load centers in Radial Distribution System (RDS). Single or multiple radial feeders are used in this development approach. Basically, the RDS entire power losses can be reduced by reducing the branch power flow or transported electrical power from transmission systems (i.e. some percentage of loads is locally meeting by local DG). To find the total power loss of the system or each feeder branch and the maximum voltage difference are found by performing load flow. The forward/backward sweep load flow analysis is used in this case. The impedance of a feeder is calculated by the specific resistance and reactance of the conductors used in the branch construction. The forward/backward sweep load flow analysis consist two steps (i) Backward sweep and (ii) Forward sweep.

Backward sweep: In this step, the load current of each node of a distribution system having $N$ number of nodes is calculated as:
$\bar{I}_{L}(m)=\left\{\frac{P_{L}(m)-j Q_{L}(m)}{\bar{V}^{*}(m)}\right\} \quad[m=1,2,3 \ldots \ldots \ldots N]$
Where, $\mathrm{P}_{\mathrm{L}}(\mathrm{m})$ and $\mathrm{Q}_{\mathrm{L}}(\mathrm{m})$ represent the active and reactive power demand at node $m$ and the phasor quantities, such as $\bar{I}_{L}, \square$ *then, the current in each branch of the system is determined as:

$$
\begin{equation*}
\bar{I}(m n)=\bar{I}_{L}(n)+\sum_{m \in \Gamma} \bar{I}_{L}(m) \tag{2}
\end{equation*}
$$

Where, the set $\Gamma$ consists of all nodes which are placed beyond the node $n$.

Forward sweep: This step is used after the backward sweep so as to calculate the voltage at each node of a distribution system as follows:
$\bar{V}(n)=\bar{V}(m)-\bar{I}(m n) Z(m n)$

Where, nodes $n$ and $m$ represent the receiving and sending end nodes respectively for the branch $m n$ and $\mathrm{Z}(\mathrm{mn})$ is the impedance of the branch.

### 2.0 BACKWARD/FORWARD SWEEP ALGORITHM

This analysis includes two steps: the backward sweep and the forward sweep. In backward sweep, voltage and currents are calculated using KVL and KCL from the outermost node. In forward sweep, the downstream voltage is computed starting from source node. The input data of this algorithm is given by node-branch oriented data. Basic data required are, active and reactive powers, nomenclature for sending and receiving nodes. Listed below summarize main steps of the proposed solution algorithm with suitable equations.

1) Assume the source voltage is load end voltage.
2) Determine branch currents and node voltages by using Kirchhoff's current and Kirchhoff's voltage laws respectively. $\mathrm{I}=(\mathrm{S} / \mathrm{V})^{*}$ : Node Voltage $=(\mathrm{V}+\mathrm{IZ})$
3) In Back sweep starting from last node and determine all branch currents and node voltages.
4) Compute new voltage with rated voltage.
5) If node voltage is in tolerance limits and print results else forward sweep.
6) Now in forward sweep calculate voltages i.e. $V_{\text {new }}=(\mathrm{V}-\mathrm{IZ})$.
7) Compute the calculated end voltage with rated voltage.
8) If the difference exceed tolerance again starts backward sweep.
9) Thus forward and backward sweep continues till within the tolerance.
10) Print the voltage magnitude at all the nodes, the real and reactive power losses at all the nodes.

### 3.0 SIMULATION RESULTS

The first test case for the proposed method is a 33-bus radial distribution system. The single line diagram is shown in Figure 4 The base values of the system are taken as 12.66 kV and 100MVA.


Voltage magnitude and phase angle, active and Reactive line losses of 33 bus system

| TABLE 1 |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| VOLTAGE MAGNITUDE AND PHASE ANGLE, ACVTIVE AND REACTIVE LINE LOSSES OF 33 BUS SYSTEM |  |  |  |  |  |  |
| $\begin{gathered} \text { S } \\ \text { no } \end{gathered}$ | Voltage magnitude | Phase angle | $\begin{array}{\|c} \text { Send- } \\ \text { ing } \\ \text { End } \end{array}$ | Re-ceiving End | Active loss KW | Reactive loss KVAR |
| 1 | 1.0000 | 0 | 1 | 2 | 12.2404 | 6.2397 |
| 2 | 0.9970 | 0.0145 | 2 | 3 | 51.7912 | 26.3789 |
| 3 | 0.9829 | 0.0960 | 3 | 4 | 19.9005 | 10.1351 |
| 4 | 0.9755 | 0.1617 | 4 | 5 | 18.6989 | 9.5237 |
| 5 | 0.9681 | 0.2283 | 5 | 6 | 38.2486 | 33.0180 |
| 6 | 0.9497 | 0.1339 | 6 | 7 | 1.9145 | 6.3285 |
| 7 | 0.9462 | -0.0965 | 7 | 8 | 4.8380 | 1.5988 |
| 8 | 0.9413 | -0.0604 | 8 | 9 | 4.1805 | 3.0035 |
| 9 | 0.9351 | -0.1335 | 9 | 10 | 3.5609 | 2.5240 |
| 10 | 0.9292 | -0.1960 | 10 | 11 | 0.5537 | 0.1831 |
| 11 | 0.9284 | -0.1888 | 11 | 12 | 0.8811 | 0.2914 |
| 12 | 0.9269 | -0.1773 | 12 | 13 | 2.6662 | 2.0978 |
| 13 | 0.9208 | -0.2686 | 13 | 14 | 0.7292 | 0.9598 |
| 14 | 0.9185 | -0.3473 | 14 | 15 | 0.3570 | 0.3177 |
| 15 | 0.9171 | -0.3850 | 15 | 16 | 0.2815 | 0.2055 |
| 16 | 0.9157 | -0.4082 | 16 | 17 | 0.2516 | 0.3360 |
| 17 | 0.9137 | -0.4855 | 17 | 18 | 0.0531 | 0.0417 |
| 18 | 0.9131 | -0.4951 | 18 | 19 | 0.1610 | 0.1536 |
| 19 | 0.9965 | 0.0037 | 19 | 20 | 0.8322 | 0.7499 |
| 20 | 0.9929 | -0.0633 | 20 | 21 | 0.1008 | 0.1177 |
| 21 | 0.9922 | -0.0827 | 21 | 22 | 0.0436 | 0.0577 |
| 22 | 0.9916 | -0.1030 | 22 | 23 | 3.1816 | 2.1740 |
| 23 | 0.9794 | 0.0651 | 23 | 24 | 5.1437 | 4.0617 |
| 24 | 0.9727 | -0.0237 | 24 | 25 | 1.2875 | 1.0074 |
| 25 | 0.9694 | -0.0674 | 25 | 26 | 2.6009 | 1.3248 |
| 26 | 0.9477 | 0.1733 | 26 | 27 | 3.3290 | 1.6950 |
| 27 | 0.9452 | 0.2295 | 27 | 28 | 11.3009 | 9.9637 |
| 28 | 0.9337 | 0.3124 | 28 | 29 | 7.8333 | 6.8242 |
| 29 | 0.9255 | 0.3903 | 29 | 30 | 3.8957 | 1.9843 |
| 30 | 0.9220 | 0.4956 | 30 | 31 | 1.5936 | 1.5750 |
| 31 | 0.9178 | 0.4112 | 31 | 32 | 0.2132 | 0.2485 |
| 32 | 0.9169 | 0.3881 | 32 | 33 | 0.0132 | 0.0205 |
| 33 | 0.9166 | 0.3804 | Total | osses | 202.6771 | 135.1410 |

The second test case for the proposed method has been tested on 69 bus Radial Distribution System, using MATLAB. 69 bus systems are shown in Figure 5. This system is consisting of 69 nodes and 65 branches, 1 reference node, KVA is 100. The tolerance is 0.00001 p.u. Results are shown in Table 2. Bus voltage magnitude in p.u. and phase angle in degree at each bus and real and reactive line losses in each branch in KW and KVAR are shown in Table 2.

## 69 BUS SYSTEM OUTPUT DATA:

Voltage magnitude and Phase angle, Active and Reactive line losses of 69 bus system


| TABLE 2 |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| VOLTAGE MAGNITUDE AND PHASE ANGLE, ACTIVE AND REACTIVE LINE LOSSES OF 69 BUS SYSTEM |  |  |  |  |  |  |
| S no | Voltage magnitude | Phase angle | Sending End | Receiving End | Active loss (KW) | Reactive loss (KVAR) |
| 1 | 1.0000 | 0 | 1 | 2 | 0 | 0 |
| 2 | 1.0000 | 0 | 2 | 3 | $3.8427 \mathrm{e}-006$ | $9.2225 \mathrm{e}-006$ |
| 3 | 1.0000 | -0.0000 | 3 | 4 | $4.8788 \mathrm{e}-007$ | $1.1709 \mathrm{e}-006$ |
| 4 | 1.0000 | -0.0000 | 4 | 5 | $3.5021 \mathrm{e}-004$ | $4.1021 \mathrm{e}-004$ |
| 5 | 1.0000 | -0.0002 | 5 | 6 | 0 | 0 |
| 6 | 1.0000 | -0.0002 | 6 | 7 | 0.0028 | 0.0015 |
| 7 | 0.9999 | 0.0006 | 7 | 8 | 0.4644 | 0.2368 |
| 8 | 0.9993 | 0.0048 | 8 | 9 | 0.2282 | 0.1162 |
| 9 | 0.9990 | 0.0070 | 9 | 10 | 3.4987 | 1.1564 |
| 10 | 0.9947 | 0.0776 | 10 | 11 | 0.4906 | 0.1622 |
| 11 | 0.9940 | 0.0900 | 11 | 12 | 0.9751 | 0.3223 |
| 12 | 0.9919 | 0.1229 | 12 | 13 | 1.3552 | 0.4473 |
| 13 | 0.9889 | 0.1699 | 13 | 14 | 1.3155 | 0.4347 |
| 14 | 0.9859 | 0.2167 | 14 | 15 | 1.3331 | 0.4405 |
| 15 | 0.9829 | 0.2644 | 15 | 16 | 0.1904 | 0.0629 |
| 16 | 0.9824 | 0.2722 | 16 | 17 | 0.2443 | 0.0808 |
| 17 | 0.9816 | 0.2850 | 17 | 18 | 0.0019 | $6.3817 \mathrm{e}-004$ |
| 18 | 0.9816 | 0.2851 | 18 | 19 | 0.1307 | 0.0432 |
| 19 | 0.9811 | 0.2945 | 19 | 20 | 0.0832 | 0.0273 |
| 20 | 0.9808 | 0.3005 | 20 | 21 | 0.0254 | 0.0084 |
| 21 | 0.9805 | 0.3048 | 21 | 22 | $9.2379 \mathrm{e}-004$ | $3.0353 \mathrm{e}-004$ |
| 22 | 0.9805 | 0.3049 | 22 | 23 | 0.0105 | 0.0035 |
| 23 | 0.9804 | 0.3068 | 23 | 24 | 0.0099 | 0.0033 |
| 4 | 0.9803 | 0.3095 | 24 | 25 | 0.0214 | 0.0071 |
| 25 | 0.9799 | 0.3152 | 25 | 26 | 0.0049 | 0.0016 |
| 26 | 0.9798 | 0.3170 | 26 | 27 | 0.0012 | $3.7991 \mathrm{e}-004$ |
| 27 | 0.9798 | 0.3177 | 27 | 28 | $3.4690 \mathrm{e}-004$ | $8.5148 \mathrm{e}-004$ |
| 28 | 1.0000 | -0.0003 | 28 | 29 | 0.0026 | 0.0063 |
| 29 | 0.9999 | -0.0029 | 29 | 30 | 0.0161 | 0.0053 |
| 30 | 0.9997 | 0.0007 | 30 | 31 | 0.0028 | $9.3670 \mathrm{e}-004$ |
| 31 | 0.9997 | 0.0013 | 31 | 32 | 0.0142 | 0.0047 |
| 32 | 0.9995 | 0.0044 | 32 | 33 | 0.0209 | 0.0070 |


| 33 | 0.9992 | 0.0102 | 33 | 34 | 0.0164 | 0.0164 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 34 | 0.9988 | 0.0175 | 34 | 35 | 0.0094 | 0.0031 |
| 35 | 0.9985 | 0.0228 | 35 | 36 | 0.0010 | 0.0025 |
| 36 | 1.0000 | -0.0005 | 36 | 37 | 0.0105 | 0.0257 |
| 37 | 0.9998 | -0.0058 | 37 | 38 | 0.0173 | 0.0202 |
| 38 | 0.9997 | -0.0082 | 38 | 39 | 0.0034 | 0.0039 |
| 39 | 0.9996 | -0.0088 | 39 | 40 | $1.2035 \mathrm{e}-004$ | $1.4041 \mathrm{e}-004$ |
| 40 | 0.9996 | -0.0089 | 40 | 41 | 0.0472 | 0.0552 |
| 41 | 0.9990 | -0.0197 | 41 | 42 | 0.0201 | 0.0235 |
| 42 | 0.9987 | -0.0244 | 42 | 43 | 0.0023 | 0.0027 |
| 43 | 0.9986 | -0.0250 | 43 | 44 | $5.1343 \mathrm{e}-004$ | $6.4737 \mathrm{e}-004$ |
| 44 | 0.9986 | -0.0251 | 44 | 45 | 0.0015 | 0.0019 |
| 45 | 0.9986 | -0.0260 | 45 | 46 | 0 | 0 |
| 46 | 0.9986 | -0.0260 | 46 | 47 | 0.0254 | 0.0627 |
| 47 | 0.9999 | -0.0019 | 47 | 48 | 0.5276 | 1.2915 |
| 48 | 0.9988 | -0.0447 | 48 | 49 | 0.4959 | 1.2133 |
| 49 | 0.9966 | -0.1214 | 49 | 50 | 0.0013 | 0.0031 |
| 50 | 0.9966 | -0.1235 | 50 | 51 | $5.8933 \mathrm{e}-005$ | $3.0038 \mathrm{e}-005$ |
| 51 | 0.9993 | 0.0049 | 51 | 52 | $6.4642 \mathrm{e}-005$ | $2.1697 \mathrm{e}-005$ |
| 52 | 0.9993 | 0.0051 | 52 | 53 | 4.0835 | 2.0793 |
| 53 | 0.9967 | 0.0255 | 53 | 54 | 4.6052 | 2.3457 |
| 54 | 0.9940 | 0.0469 | 54 | 55 | 6.2458 | 3.1800 |
| 55 | 0.9903 | 0.0764 | 55 | 56 | 6.1820 | 3.1493 |
| 56 | 0.9866 | 0.1059 | 56 | 57 | 34.9428 | 11.7289 |
| 57 | 0.9678 | 0.4333 | 57 | 58 | 17.2231 | 5.7799 |
| 58 | 0.9585 | 0.5995 | 58 | 59 | 5.8008 | 1.9184 |
| 59 | 0.9552 | 0.6610 | 59 | 60 | 7.3626 | 2.2349 |
| 60 | 0.9510 | 0.7454 | 60 | 61 | 0.0631 | 0.0321 |
| 61 | 0.9505 | 0.7499 | 61 | 62 | 0.0060 | 0.0031 |
| 62 | 0.9505 | 0.7505 | 62 | 63 | 0.1399 | 0.0712 |
| 63 | 0.9501 | 0.7541 | 63 | 64 | 0.0440 | 0.0224 |
| 64 | 0.9496 | 0.7585 | 64 | 65 | 0.0036 | 0.0018 |
| 65 | 0.9494 | 0.7601 | 65 | 66 | 0.0041 | 0.0012 |
| 66 | 0.9939 | 0.0914 | 66 | 67 | $3.5147 \mathrm{e}-00$ | $1.0469 \mathrm{e}-005$ |
| 67 | 0.9939 | 0.0914 | 67 | 68 | 0.0056 | 0.0018 |
| 68 | 0.9917 | 0.1258 | 68 | 69 | 0 | 0 |
| 69 | 0.9917 | 0.1258 | Total losses |  | 98.3377 KW | 38.8593 KVAR |

### 4.0 CONCLUSION

This method for solving the load flow problem for radial distribution uses simple algebraic equations to determine iteratively the outgoing powers and voltage magnitudes of various nodes and mismatches at the last nodes of main feeder and laterals and depending upon mismatches the substation injection is corrected judiciously and this process is repeated until convergence. The total active and reactive power losses for 33 KV and 69 KV system are $202.6771 \mathrm{KW}, 135.1410$ KVAR and 98.3377 KW, 38.8593 KVAR
respectively. This makes the algorithm very robust and numerically efficient for convergence for wide variation of distribution network determines the behavior of the entire system.

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